

**Magnet Arrangement for Carrying, Guiding and/or Braking Systems in  
Magnetic Levitation Vehicles**

The present invention relates to a magnet arrangement according to the species designated in the preamble of Claim 1.

With magnet arrangements of this kind (DE 34 10 119 C2), the cores, particularly  
5 those destined for carrier magnets, are comprised of a plurality of plates or sheets  
compiled to form a sheet metal pack, thus leading to a low intrinsic attenuation for the  
magnet arrangement as a whole. Moreover, the windings of the coils in most cases  
are formed by conductor strips wound around the core and connected to each other  
in alternating succession at their ends located radially outside away from the core  
10 and radially inside near the core. This results in numerous parasitary longitudinal and  
transverse capacities between the individual layers of the windings and/or between  
the layers radially located farthest inside and the core, which together with the  
inductivities (inductances) of the windings form electrical resonant circuits. Due to the  
low intrinsic attenuation during excitation of the magnet arrangement, these resonant  
15 circuits lead to electrical oscillations and excessive voltage rates at critical points of  
the magnet arrangement, particularly when reaching the relevant resonance  
frequency ranges.

Voltage overshoots involve particularly adverse effects at those points of the magnet  
20 arrangement where the innermost layers of two adjacent windings lying nearest to  
the relevant core are electrically connected with each other by internal connection  
lines. The resulting voltages and/or electric currents might be so high that the  
insulation layers arranged between the first layers and the core are destroyed, thus  
rendering the entire magnet arrangement useless.

25 To avoid insulation damage it would be possible to rate the space between the cores  
and the relevant first winding layers large enough in radial direction and/or to provide  
the inner insulation layers with an adequate thickness. However, this would entail a  
disadvantage in that the heat loss generated in the coils could not be dissipated any

longer radially via the cores acting as cooling elements, thus deteriorating the cooling efficiency noticeably. On the other hand, the spaces mentioned before would no longer be available for the windings, thus reducing the space factors.

5 In practice, the oscillations occurring with magnet arrangements of the species designated hereinabove are attenuated by resistors connected in parallel to the coils and forming a passive attenuation network. However, such a network entails a significant drawback in that the resistors generate quite a substantial heat loss and therefore have to be cooled with ambient air, which is difficult to accomplish, and  
10 moreover, these resistors would have to be made of high-grade quality materials to safely avoid any damage during operation. This would substantially increase the cost expenditure for the magnet arrangement.

Now, therefore and in consideration hereof, it is the object of the present invention to  
15 configure the magnet arrangement of the species as designated hereinabove in such a manner that the oscillations as described can be reduced and/or rendered harmless even without applying any ohmic resistors.

The characterizing features of Claim 1 serve to solve this object.

20 The present invention yields an advantage in that the resonances occurring on excitation of the magnet arrangement are noticeably attenuated by the aid and/or application of the pole backs existing in any way or in that the voltage and/or electrical current overshoots caused by them are so compensated that insulation  
25 damage is effectively avoided.

Other advantages of the present invention become evident from the subclaims.

The present invention is explained in more detail hereinafter in conjunction with  
30 embodiments and based upon the appending drawings, in which

FIG. 1 shows a schematic section through a magnet arrangement for magnetic levitation vehicles with long stator drive;

Fig. 2 shows a schematic view of a substitute circuit diagram for the magnet arrangement according to FIG. 1;

5 FIG. 3 shows graphs for the resonant oscillations occurring on excitation of the magnet arrangement according to FIG. 1 and 2;

FIG. 4 and 5 each show a section according to FIG. 1 through a first and a second embodiment of a magnet arrangement according to the present invention;

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FIG. 6 shows a diagram with attenuation curves obtained when implementing the embodiment according to FIG. 4 and 5; and

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FIG. 7 and 8 show sections according to FIG. 1 through another two embodiments of the magnet arrangement according to the present invention.

According to FIG. 1, the iron body of a conventional magnet arrangement 1, e.g. configured as a carrier magnet and suitable for magnetic levitation vehicles equipped with a long stator drive, is provided with a meander-like cross-section in a longitudinal direction defined by a longitudinal axis 2. Several, here six cores 3a to 3f, arranged at a certain distance from each other, are magnetically connected to each other at their underside through one so-called pole back 4 each, with the cores 3 and the pole backs 4 usually being connected to ground. Between the cores 3a to 3f and above the pole backs 4, the magnet arrangement 1 is provided with grooves running transversely to the longitudinal axis 2 and having rectangular cross-sections, and in which coils 5a to 5f wound around allocated cores 3a and 3f are arranged. Coils 5a to 5f consist of conductor strips not shown which have a width that corresponds to the height of the grooves and which are wound in close contact to each other around said cores 3a to 3f.

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Insulation layers not shown are provided between the individual layers of the conductor strips, and another insulation layer 6a to 6f each is provided between the relevant layers radially located farthest inside and the relevant cores 3a to 3f.

Moreover, the radially outermost layers of the coils 5a, 5b, and 5c, 5d and 5e, 5f, respectively are electrically connected to each other through external connection lines 7, while the radially innermost layers of the coils 5b, 5c and 5d, 5e, respectively, are electrically connected to each other through internal connection lines 8, so that  
 5 the internal and external connection lines 7, 8 alternate each other in longitudinal direction. Finally, excitation of the magnet arrangement 1 is accomplished by way of an electric current converter (chopper) 9 which is connected to the innermost layer of coil 5a, while the innermost layer of coil 5f is connected to ground. The cores 3a to 3f together with the pertaining coils 5a to 5f form one magnet pole each with alternating  
 10 polarity in the direction of longitudinal axis 2.

The equivalent circuit diagram for the magnet arrangement 1 according to FIG. 1 is shown in FIG. 2, with equal parts being designated by the same reference numbers. It becomes evident thereof that in parallel to the individual coils 5a to 5f and formed  
 15 by their layers, longitudinal capacities 10 exist being arranged in series. Moreover, at those points where the innermost layers of coils 5b, 5c and 5d, 5e respectively are connected to each other by the connection lines 7, there is a comparably great transverse capacity 11 and 12 respectively, each leading to the pertaining core connected to ground, and at those points where the innermost layers of the coils 5a,  
 20 5f have a connection extending from the innermost layer to the outside, there is a transverse capacity 14, 15 each being roughly half as big as the capacity 11 or 12 and leading to the ground.

On account of this arrangement, the coils or inductivities 5a to 5f form together with  
 25 the capacities 10 and 11 to 15 an oscillating circuit in which electrical oscillations are generated on excitation of the magnet arrangement 1 by means of the electric current converter 9, said electrical oscillations for example having two resonance frequencies depending on the layout of the magnet arrangement 1 and being indicated by two peaks 16 and 17 underneath the equivalent circuit diagram in Fig. 2.

30 A particularly critical behavior at these frequencies demonstrate two connecting points 18 and 19 being arranged between the coils 5b, 5c on the one hand and 5d, 5e (FIG. 2) on the other hand, and leading to ground via the capacities 11, 12. At

these points, as shown on FIG. 1, the innermost layers of coils 5b, 5c and 5d, 5e are connected to each other. If the insulation 6 at these points disrupts towards the relevant core 3 and/or towards the ground, a short-circuit will occur and thus render the magnet arrangement 1 useless. Contrary, other switching points are comparably

5 uncritical, e.g. points where the coils 5a, 5b and 5c, 5d etc. are connected externally, as well as the connecting points which are linked to capacities 14 and 15. A consequence of this all is that the voltage rates at the connecting points 18 and 19 rise substantially at the resonance frequencies according to FIG. 2 and that the electric currents through the adjacent coils 5b, 5c and 5d, 5e, respectively, adopt

10 very different values. For example, this becomes evident from the measuring curves shown in FIG. 3, in which the time is plotted along the abscissa and wherein the electrical current is plotted along the ordinate. As shown at the top and on the left side of FIG. 3, a curve 21 represents the electrical current flowing through coil 5b and a curve 22 represents the electrical current flowing through coil 5c in case that the

15 circuitry according to FIG. 2 is excited by means of electric current converter 9 with a sinusoidal voltage near the one resonance frequency (Peak 16) in FIG. 2. Correspondingly, curves 23, 24 are shown at the top on the right side for the electrical currents flowing at the same frequency in coils 5e and 5d. In the bottom part of FIG. 3, curves 25, 26 and 28, 29 show the behavior of electrical currents when

20 excitation is accomplished with a frequency which lies near the resonance frequency indicated by peak 17 in FIG. 2. From FIG. 3 it follows that the electrical currents through the coils 5b, 5c and 5d, 5e and, consequently, the electrical currents flowing to the connecting points 18, 19 and/or the electrical currents flowing from these connecting points 18, 19 differ substantially from each other. Moreover, the electrical

25 currents at resonance frequency according to peak 17 are phase-shifted by 180° each (curves 26, 27 and 28, 29, respectively). Because voltages in a magnitude of  $10^4$  V as compared to conventional operating voltages of approximately 440V may occur, differential currents flow via the capacities 11 and 12, thus entailing the danger of disrupting the insulation.

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Hence, it is attempted in accordance with the present invention to attenuate the oscillating circuit, and particularly to reduce or adapt to each other the electrical currents flowing through coils 5b, 5c on the one hand and 5d, 5e on the other hand

so as to avoid harmful consequences from resonance. The idea being behind this approach is that the pole backs (FIG. 1) themselves which are existing in any case may be used as essential means for attenuation and/or compensation.

5 With the embodiment according FIG. 4 it is proposed to manufacture selected pole backs 4 from a material having high eddy current losses and/or preferably from massive components rather than of individual sheet metal lamellae. Since the individual coils 5a to 5f are magnetically coupled to each other via the iron cores 3 and pole backs 4, eddy currents in the pole backs 4 automatically lead to a dynamic  
10 attenuation. Minor heat losses occurring due to these eddy currents are dissipated via the continuous iron body of the magnet arrangement 1, particularly if pole backs 4 are of a massive structure. The electrical currents flowing off from the connecting points 18, 19 via capacities 11, 12 can be substantially reduced in this manner. Consequently, the maximum voltages occurring at the connection points 18, 19 are  
15 so low that they range by far under the disruptive voltages for the relevant insulation layers.

The same applies if selected pole backs 4 according to FIG. 5 are wrapped with at least one short-circuit winding 30 each. In particular it may be expedient not to  
20 fabricate these short-circuit windings 30 from high-grade conductors, e.g. copper or aluminum, but for example from iron in order to generate high energy losses by them and thus to cause an effective dynamic attenuation.

With both the embodiments pursuant to FIG. 4 and 5, all the existing pole backs 4  
25 also constitute selected pole backs 4 as all pole backs 4 are configured in the same way.

Moreover, both embodiments of FIG. 4 and 5 work passively. The embodiment according to FIG. 4 works in the manner of a low-pass filter, leading to an attenuation  
30 curve 31 according to FIG. 6. The embodiment pursuant to FIG. 5, on the contrary, works in the manner of a band-pass filter, leading to an attenuation curve 32 in FIG. 6. Both attenuation curves 31, 32 encompass the resonance frequencies 16 and 17.

The embodiments according to FIG. 7 and 8 in conformity with the present invention show active arrangements for reducing the resonant oscillations occurring in coils 5. In accordance with FIG. 7, it is envisaged to equip selected pole backs 4a, 4b, and 4c, which establish a connection among cores 3a, 3b and 3c, 3d and 3e, 3f, respectively, with a compensation coil 34 each, and to establish a galvanic connection among these three compensation coils 34 in a series circuitry. The arrangement is so chosen that the flow into the pole back 3a and 3b and 3b and 3c each is basically equivalent. As the flow into the pole backs 4d and 4e, which are not provided with a compensation coil 34, influences the pertaining coils 5b and 5c (5d and 5e, respectively) in the same manner, the arrangement as described hereinabove involves that the flows through coils 5b and 5c on the one hand and 5d and 5e on the other hand are basically equivalent. Thereby it can be achieved that at least the electric current peaks occurring in the coils in case of resonance are adapted to each other and the voltage overshoots at the connecting points 18, 19 in FIG. 2 are reduced to such an extent that the electric currents flowing off via the capacities 11, 12 are uncritical.

Besides, an advantage of the embodiments working with short-circuit coils and/or compensation coils 30, 34 is that an adaptation to the resonance frequencies prevailing in a given case can be accomplished by choosing the proper coil parameters. The same applies by analogy to the embodiment of FIG. 8, where a transformer generally designated with reference number 25 is switched between the compensation coils 4. Here, too, the phase angle of the electrical currents generated by induction in the windings 34 and/or the secondary electrical currents discharged from transformer 35 shall be so chosen that the desired compensation efficiency is obtained. In contrast with FIG. 7, transformation ratios that differ from 1:1 can be adjusted and set by transformer 35. Besides, it is also advantageous to apply sheet metal packets composed of individual lamellae for the pole backs 4 of the embodiments according to FIG. 5 to 8.

The present invention is not limited to the embodiments described herein that can be varied in a plurality of ways. In particular, this applies to the intended application of

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the magnet arrangement 1 as described hereinabove, which could also be applied in guiding or braking magnets, if required. Furthermore, the invention is not limited to coil windings made of flat conductor strips, but by analogy can also be applied to coils with different windings, if the attenuation with these coils is comparably low. The  
5 number of magnet poles and/or cores 3 existing per magnet arrangement 1 can also be chosen largely at will. Finally, it is considered self-evident that the different characteristic features can also be applied in combinations other than those shown and described hereinabove.